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# Short Communication





# Further Analysis on Solubility Measurement and Thermodynamic Modeling of Benzoic Acid in Monosolvents and Binary Mixtures

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# ABSTRACT

**Background:** Recently Sandeepa et al. reported the solubility of benzoic acid in six monosolvents (i.e. tributyl phosphate, diacetone alcohol, methyl-n-propyl ketone, methyl acetate, amyl acetate, and isooctane) and five binary systems (i.e. ethanol + hexane, isopropyl alcohol + hexane and chloroform + hexane, acetone + hexane, and acetone + water) along with some numerical analyses. The reported calculations have been reanalyzed and some recommendations and further computations were proposed.

*Methods:* Further analyses were performed based on combined nearly ideal binary solvent/Redlich-Kister, the modified Wilson model, general single model, Jouyban–Acree model and Jouyban–Acree–van't Hoff model.

*Results:* The mentioned numerical analyses were used to predict the solubility of benzoic acid in the binary solvent mixtures at various temperatures and the predicted solubility data were compared with their corresponding experimental values by calculating relative deviations.

*Conclusion:* The investigated models provide good estimation of the solubility behavior of benzoic acid in the binary solvent mixtures at various temperatures.

#### Introduction

In a recently published paper, Sandeepa et al.<sup>1</sup> reported the experimental solubility of benzoic acid in a number of mono-solvents including tributyl phosphate, diacetone alcohol, methyl-n-propyl ketone, methyl acetate, amyl acetate, and isooctane and five binary solvent systems (i.e. ethanol + hexane, isopropyl alcohol + hexane and chloroform + hexane, acetone + hexane, and acetone + water) at various temperatures along with some numerical analyses. Benzoic acid is used as an antimicrobial food additive to prevent the proliferation of bacteria, yeasts and moulds.<sup>2</sup> Benzoic acid was used as an expectorant, analgesic, and antiseptic in the early 20th century.<sup>3</sup> It can be used for the treatment of fungal skin diseases such as tinea, ringworm, and athlete's foot.<sup>4</sup> Benzoic acid is an important precursor for the industrial synthesis of many other organic substances. Therefore, its solubility determination and prediction in neat solvents or mixed systems can be useful for separation and purification of benzoic acid from reaction media. The generated experimental solubility data extends the solubility database of benzoic acid in mono-solvents and the mixed solvents and could be helpful in the pharmaceutical and chemical industries. In addition to experimental efforts, various numerical models proposed for the estimation of the solubility of drug and/or drug like compounds<sup>5</sup> in the mono-solvents and the cosolvency systems include the van't Hoff equation, Apelblat, and Buchowski ( $\lambda$ h) models. the mixture response surface, the phenomenological model, the non-random two-liquid model (NRTL) model, the combined nearly ideal binary solvent/Redlich-Kister equation, the modified Wilson model, fluctuation theory, and the Jouyban-Acree model. Sandeepa et al.<sup>1</sup> correlated the experimental solubility data of benzoic acid in the binary solvent mixtures using the Ah equation, the NRTL model, and the modified Apelblat-Jouyban-Acree model for aqueous binary solvent mixtures. Further analyses were performed in this study which provide more information for better understanding of the solubility behavior of benzoic acid in the investigated solvents.

# **Results and Discussion**

At first, the reported calculations on solubility data of benzoic acid were reanalyzed. Sandeepa *et al.*<sup>1</sup> have correlated the mole fraction solubility data of benzoic acid in binary solvent systems at different temperatures with the  $\Lambda$ h equation expressed as:

$$x = \frac{\lambda}{e^{\lambda h(T^{-1} - T_m^{-1})} - 1 + \lambda}$$
 Eq. (1)

where x is the mole fraction solubility at temperature T;

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 $T_m$  is the melting point of the solute.  $\lambda$  and h are the coefficients of model.

The accuracy of the computations were assessed using the relative deviation (RD) defined as

$$RD = \frac{1}{N} \sum \left( \frac{\left| x^{\exp} - x^{\operatorname{cal.}} \right|}{x^{\exp}} \right)$$
 Eq. (2)

and root mean square deviation (RMSD) as

$$RMSD = \sqrt{\frac{\sum (x^{\text{exp.}} - x^{\text{cal.}})^2}{N}}$$
Eq. (3)

where N is the number of experimental points,  $x^{cal}$  is the

calculated solubility and  $x^{exp.}$  is the experimental solubility.

The recalculated parameters for Eq. 1 by SPSS software version 16.0,<sup>6</sup> show an inconsistency for constants and *RD* obtained for all investigated systems. A comparison between reported data (Table 5 of the published paper) and our recalculated data is summarized in Table 1. However, the aim of this short communication is not to criticize valuable work of Sandeepa *et al.*, but rather is to report further calculations and to provide predictive computations.

**Table 1.** Recalculated parameters of the  $\lambda$ h equation (Eq. 4 of the published paper) for describing the solubility of benzoic acid in ethanol (1) + hexane (2) solvent mixtures.

Wa <sup>1</sup>		Paramete Table 5 Re		Parameters (recalculated data)			
	٨	h	100RD	٨	h	100RD	
0.200	1.33	2755.10	1.26	0.732	1309	7.98	
0.360	1.99	1796.16	2.06	0.920	2136	2.65	
0.491	1.53	1975.27	0.81	0.941	2118	1.74	
0.600	1.19	2135.63	0.79	0.968	2149	0.63	
0.693	1.22	2027.23	1.29	0.950	1965	0.94	
0.772	0.81	2349.37	1.51	0.847	1355	1.31	
0.840	0.64	2509.70	0.80	0.832	1240	1.36	
0.900	0.63	2485.36	1.02	0.829	1200	0.80	

 ${}^{1}\textit{w}_{a}$  is the mole fraction of ethanol in the mixtures with water in the absence of solute.

In addition to the correlative models employed by Sandeepa et al.,<sup>1</sup> one may use the combined nearly ideal binary solvent/Redlich-Kister (CNIBS/R-K),<sup>7</sup> the modified Wilson<sup>8</sup> and general single models (GSM).<sup>9</sup> The models are

$$\ln x_m = w_1 \ln(x_1)_B + w_2 \ln(x_1)_C + w_1 w_2 \sum_{i=0}^2 J_i (w_1 - w_2)^i$$
Eq. (4)

$$-\ln x_{m}^{scat} = 1 - \frac{w_{1}[1 + \ln(x_{1})]}{w_{1} + w_{2}\lambda_{12}} - \frac{w_{2}[1 + \ln(x_{2})]}{w_{1}\lambda_{21} + w_{2}}$$
  
Eq. (5)

$$\ln x_{m} = B_{0} + B_{1}x_{b} + B_{2}(x_{b})^{2} + B_{3}(x_{b})^{3} + B_{4}(x_{b})^{4}$$
Eq. (6)

The CNIBS/R-K, modified Wilson model and GSM are correlative models and produce the similar accuracies for a given solute in a certain binary solvent mixture at a constant temperature. We recommend to use the extended version (i.e. the Jouyban–Acree model and/or its combined version with the van't Hoff equation), which consider both solvent composition and temperature. The Jouyban–Acree model is one such versatile model with good predictability power over broad temperature range and solvent composition.<sup>10-12</sup> The general version of the Jouyban-Acree model is:

$$\ln x_{m,T}^{sat} = w_1 \cdot \ln x_{1,T}^{sat} + w_2 \cdot \ln x_{2,T}^{sat} + \frac{w_1 \cdot w_2}{T} \sum_{i=0}^{2} J_i \cdot (w_1 - w_2)^i$$
Eq. (7)

which correlates the solute solubility in binary solvent mixtures at various temperatures employing experimental solubility data in the mono-solvents. To cover this limitation, one may combine the model with van't Hoff equation as<sup>13,14</sup>

$$\ln x_{m,T}^{sat} = w_1 (A_1 + \frac{B_1}{T}) + w_2 (A_2 + \frac{B_2}{T}) + \frac{w_1 \cdot w_2}{T} \sum_{i=0}^2 J_i \cdot (w_1 - w_2)^i$$
Eq. (8)

where  $\mathcal{X}_{m,T}^{sat}$  is the mole fraction solubility of solute (benzoic acid in this case) in the solvent mixtures at temperature T/K,  $W_1$  and  $W_2$  are the mass fractions of mono solvents 1 and 2, in the absence of the solute, and  $A_1$ ,  $B_1$ ,  $A_2$ ,  $B_2$  and  $J_i$  are constants of the model obtained by a regression analysis.

The experimental solubility results for benzoic acid in the investigated cosolvency systems are fitted to Eqs. 4 to 8 and the applied model constants are presented in Tables 2 to 5. The solubility of benzoic acid in the each system was back-calculated on the basis of the regressed values of the model parameters. The obtained values of the *100RD* are also tabulated in Tables 2 to 5. Using these computations, the solubility at each given temperature could be calculated in the acceptable error range in pharmaceutical and industrial applications by CNIBS/R-K model, modified Wilson model, GSM, Jouyban–Acree model and Jouyban-Acree-van't Hoff model.

By incorporating the structural information about the solute and solvents in the computations, a significant improvement may be achieved for the solubility prediction of drugs in the cosolvency systems as shown in an earlier work.<sup>15</sup> The basic quantitative structure property relationship (QSPR) is:<sup>16</sup>

$$J_{i} = J_{1,i}[(c_{1} - c_{2})^{2}] + J_{2,i}[E(e_{1} - e_{2})^{2}] + J_{3,i}[S(s_{1} - s_{2})^{2}] + J_{4,i}[A(a_{1} - a_{2})^{2}] + J_{5,i}[B(b_{1} - b_{2})^{2}] + J_{6,i}[V(v_{1} - v_{2})^{2}] + J_{7,i}[A.B(a_{1}b_{1} - a_{2}b_{2})^{2}]$$
Eq. (9)

where subscripts 1 and 2 denote the cosolvent and solvent, respectively, *E* is the excess molar refraction, *S* is the dipolarity/polarizability of the solute, *A* and *B* denotes the solute's hydrogen-bond acidity and basicity, and *V* is the McGowan characteristic volume of the solute in units of  $(\text{cm}^3, \text{mol}^{-1})/100$ .

Solubility and Thermodynamic Modeling of Benzoic Acid in Monosolvents and Binary Mixtures

<i>T</i> (K)	288.15	293.15	298.15	303.15	308.15	313.15	318.15	323.15	328.15
				Ethanc	ol + Hexane				
$J_0$	4.495	4.552	4.332	4.233	4.199	4.278	4.122	4.113	4.042
$J_1$	-3.996	-3.823	-3.589	-3.323	-3.584	-3.607	-3.549	-3.586	-3.528
$J_2$	4.702	4.689	4.408	4.015	3.857	3.801	3.664	3.641	3.584
100RD	2.8	1.2	1.4	0.7	0.8	0.6	0.9	0.4	1.0
				Isopropyl a	lcohol + Hexa	ne			
$J_0$	4.655	4.608	4.380	4.273	4.274	4.223	4.111	4.084	-
$J_1$	-5.305	-5.119	-4.861	-4.809	-4.935	-4.996	-4.906	-4.921	-
$J_2$	5.417	5.125	4.809	4.679	4.737	4.581	4.412	4.313	-
100RD	0.7	0.8	1.1	0.9	0.7	0.3	0.6	0.8	-
				Chlorofo	orm + Hexane				
$J_0$	3.548	3.547	3.203	3.178	3.268	3.311	3.248	3.284	-
$J_1$	-3.269	-2.954	-3.071	-3.045	-3.000	-3.105	-3.092	-3.121	-
$J_2$	3.164	3.009	2.819	2.957	2.797	2.703	2.587	2.482	-
100RD	1.1	0.8	1.6	1.4	1.3	0.9	0.9	1.2	-
				Aceton	e + Hexane				
$J_0$	3.606	3.482	3.312	3.351	3.514	3.659	3.468	-	-
$J_1$	-3.796	-3.739	-3.674	-3.776	-3.930	-4.188	-4.173	-	-
$J_2$	4.269	4.595	4.488	4.568	4.569	4.623	4.728	-	-
100RD	1.4	0.5	0.4	1.4	1.9	3.5	3.3	-	-
				Aceto	ne + Water				
$J_0$	11.985	11.748	11.446	11.082	10.726	10.775	10.638	-	-
$\mathbf{J}_1$	-7.458	-9.266	-10.236	-9.934	-11.130	-10.352	-9.743	-	-
$J_2$	15.348	12.294	10.140	10.142	8.932	10.124	11.923	-	-
100RD	5.7	3.6	4.3	2.7	2.3	1.3	2.3	-	-

Table 2. Regression results of the CNIBS/R-K equation model.

Table 3. Regression results of the modified Wilson model.

<i>T</i> (K)	288.15	293.15	298.15	303.15	308.15	313.15	318.15	323.15	328.15
				Etha	anol + Hexane	)			
K12	0.175	0.535	0.755	1.208	1.019	1.620	2.159	3.714	8.845
$\Lambda_{21}$	5.711	5.103	5.048	4.846	5.692	6.09	6.860	7.941	10.034
100RD	5.4	5.1	5.0	4.3	3.3	3.1	2.5	2.1	1.2
				Isopropy	l alcohol + He	exane			
K12	0.152	0.132	0.122	0.113	0.098	-0.002	-4.2×10⁻ <sup>8</sup>	-5.315	-
<b>1</b> 21	6.595	7.569	8.204	8.882	10.186	12.423	7.227	8.331	-
100RD	6.4	4.3	3.4	3.0	3.4	3.7	12.97	22.6	-
				Chlore	oform + Hexa	ne			
K12	0.211	0.187	0.199	0.180	0.163	0.154	0.188	0.354	-
<b>1</b> 21	4.740	5.338	5.030	5.567	6.120	6.474	6.738	6.511	-
100RD	3.4	1.9	2.8	2.5	1.4	1.4	1.2	0.9	-
				Acet	one + Hexan	e			
<b>Л</b> <sub>12</sub>	0.253	0.231	0.216	0.186	0.157	0.130	0.118	-	-
<b>1</b> 21	3.955	4.324	4.633	5.367	6.383	7.721	8.489	-	-
100RD	8.3	7.6	7.2	6.0	4.8	4.3	4.3	-	-
				Ace	tone + Water				
<b>Л</b> <sub>12</sub>	5.307	405.970	5.0×10 <sup>7</sup>	1.5×10 <sup>7</sup>	1.5×10 <sup>7</sup>	2.479×10 <sup>7</sup>	4.1×10 <sup>7</sup>	-	-
1 <sub>21</sub>	7.008	7.199	7.789	8.145	8.561	9.188	9.9	-	-
100RD	8.7	10.4	12.58	12.6	15.2	17.2	18.2	-	-

Table 4. Regression results of the GSM.

<i>T</i> (K)	288.15	293.15	298.15	303.15	308.15	313.15	318.15	323.15	328.15
				Ethan	ol + Hexane				
$B_0$	-5.216	-4.886	-4.532	-4.278	-4.072	-3.902	-3.629	-3.448	-3.211
B <sub>1</sub>	11.667	11.335	10.602	10.086	10.219	10.226	9.824	9.761	9.449
B <sub>2</sub>	-15.335	-14.991	-14.114	-13.319	-14.104	-14.267	-13.957	-14.091	-13.817
B <sub>3</sub>	7.136	6.867	6.439	5.981	6.531	6.586	6.488	6.584	6.448
$B_4$	-	-	-	-	-	-	-	-	-
100RD	10.4	10.1	9.53	8.3	8.0	7.8	7.6	7.6	7.3
				Isopropyl a	Icohol + Hexa	ine			
$B_0$	-5.182	-4.852	-4.500	-4.241	-4.034	-3.868	-3.595	-3.414	-
B <sub>1</sub>	13.283	12.806	12.060	11.760	11.789	11.755	11.359	11.233	-
B <sub>2</sub>	-19.821	-19.261	-18.270	-18.030	-18.435	-18.622	-18.227	-18.230	-
B₃	10.020	9.684	9.183	9.092	9.360	9.520	9.333	9.353	-
$B_4$	-	-	-	-	-	-	-	-	-
100RD	12.0	11.2	10.3	10.4	10.5	10.4	9.9	9.9	-

Table 4.	(Continued)								
	, , ,			Chlorof	orm + Hexane				
$B_0$	-5.223	-4.893	-4.534	-4.271	-4.066	-3.900	-3.628	-3.446	-
$B_1$	9.636	9.121	8.716	8.543	8.509	8.654	8.434	8.426	-
B <sub>2</sub>	-12.903	-12.026	-11.945	-11.859	-11.809	-12.260	-12.152	-12.265	-
$B_3$	6.188	5.607	5.785	5.742	5.649	5.924	5.895	5.952	-
$B_4$	-	-	-	-	-	-	-	-	-
100RD	6.7	6.4	6.0	6.3	5.9	5.7	5.5	5.3	-
				Acetor	ne + Hexane				
$B_0$	-5.221	-4.872	-4.515	-4.244	-4.034	-3.851	-3.576	-	-
B <sub>1</sub>	10.849	10.382	9.882	9.795	9.981	10.217	9.80	-	-
B <sub>2</sub>	-14.585	-14.132	-13.741	-13.956	-14.516	-15.256	-15.034	-	-
$B_3$	7.234	7.008	6.863	6.981	7.242	7.641	7.617	-	-
$B_4$	-	-	-	-	-	-	-	-	-
100RD	9.8	10.2	9.7	9.6	9.7	10.1	10.2	-	-
				Aceto	ne + Water				
$B_0$	-8.244	-8.29	-7.611	-7.317	-7.187	-6.993	-6.833	-	-
$B_1$	33.875	34.001	33.047	32.222	32.770	32.503	32.651	-	-
B <sub>2</sub>	-60.807	-61.448	-59.834	-58.685	-60.580	-60.477	-61.645	-	-
$B_3$	33.344	33.751	32.779	32.252	33.841	33.625	34.588	-	-
$B_4$	-	-	-	-	-	-	-	-	-
100RD	11.2	9.2	8.3	7.0	6.8	7.7	9.2	-	-

 Table 5. Regression results of the Jouyban-Acree model and Jouyban-Acree-van't Hoff model.

		Parameters	
Jouyban-Acr		Jouyban-Acree-van't Hoff	
Ethanol + He			
$J_0$	1310.974	$A_1$	3.361
$J_1$	-1113.135	A <sub>2</sub>	10.963
$J_2$	1245.775	$\overline{B_1}$	-1510.962
-2		$B_2$	-4662.335
		$J_0^2$	1311.086
		$J_1$	-1107.479
			1249.109
100RD	1.6	J₂ 100RD	1.8
IUURD	1.0		1.0
	1000 710	Isopropyl alcohol + Hexane	4.004
Jo	1320.716	A1	4.094
$J_1$	-1519.304	$A_2$	10.972
$J_2$	1452.264	B1	-1705.927
		$B_2$	-4664.149
		$J_0$	1320.969
		$J_1$	-1512.459
		$J_2$	1456.048
100RD	1.4	100RD	1.8
		Chloroform + Hexane	
J <sub>o</sub>	1013.883	A <sub>1</sub>	6.724
$J_1$	-939.524	$A_2$	11.321
$J_2$	860.200	$B_1$	-2622.749
02	000.200	$B_2$	-4769.569
		$J_0$	1012.242
			-928.611
		$J_1$	
10000	<b>2</b> 2		858.227
100RD	2.0	100RD	2.0
		Acetone + Hexane	1.000
J <sub>o</sub>	1053.956	A <sub>1</sub>	4.398
$J_1$	-1177.063	$A_2$	12.884
$J_2$	1374.822	$B_1$	-1798.698
		$B_2$	-5239.721
		$J_0$	1053.218
		$J_1$	-1165.082
		$J_2$	1376.022
100RD	2.9	100RD	2.6
		Acetone + Water	
Jo	3392.677	A <sub>1</sub>	4.509
$J_1$	-2936.341	$A_2$	8.484
$J_2$	3421.345	$B_1$	-1830.508
•2	0121.010	$B_2$	-4863.673
			3380.286
		$J_0$	
		$J_1$	-2968.552
	1.0		3316.102
100RD	4.2	100RD	5.6

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The *c*, *e*, *s*, *a*, *b* and *v* (solvent's coefficients), which depend upon the solvent under investigation. The *e* is the tendency of the phase to interact with solutes through polarizability-type interactions, *s* is a measure of the solvent phase dipolarity/polarity, the *a*- and *b*-coefficients represent the solvent phase hydrogen-bond basicity and acidity, respectively and *v* is the general dispersion interaction energy between the solute and solvent phase. Numerical values of the coefficients for water-to-organic solvent systems have been reported in the literature <sup>17</sup> and tabulated in Table 6.

**Table 6.** The Abraham parameters of the investigated solvents taken from a reference.  $^{17}$ 

Solvent	С	е	s	а	b	V
2-Propanol	0.099	0.343	-1.049	0.406	-3.827	4.033
Ethanol	0.222	0.471	-1.035	0.326	-3.596	3.857
Acetone	0.313	0.312	-0.121	-0.608	-4.753	3.942
Hexane	0.333	0.560	-1.710	-3.578	-4.939	4.463
Chloroform	0.191	0.105	-0.403	-3.112	-3.514	4.395
Water	-0.994	0.577	2.549	3.813	4.481	-3.869

By simplifying of Eq. 9 for a given drug/drug like compound, the Jouyban-Acree-van't Hoff model combined with the Abraham parameters of solvent coefficients for calculating the solubility in mixed solvents at various temperatures is expressed as Eq. 10. The *J* terms are the model constants computed using a no intercept least square analysis.

All obtained solubility data of benzoic acid in the binary solvent mixtures at various temperatures were fitted to Eq. 10 and the trained version of Jouyban-Acree-van't Hoff model combined with the Abraham parameters of solvent coefficients, as a QSPR model, after excluding nonsignificant model constant (p>0.05) is Eq.11.

The back-calculated *MRDs%* are 8.5% for solubility of benzoic acid in {ethanol (1) + hexane (2)} mixture, 10.7% in {isopropyl alcohol (1) + hexane (2)} mixture, 13.6% in {chloroform (1) + hexane (2)} mixture, 11.8% in {acetone (1) + hexane (2)} mixture and 157.7% in {acetone (1) + water (2)} mixture. The overall predicted *MRD%* is 35.2%.

# Conclusion

In addition to reanalyzing of mathematical computations published by Sandeepa *et al.*, some further computational methods are also provided in this short communication to be employed in the future research works. Furthermore, discussions regarding the Jouyban–Acree–van't Hoff model and its combined version with the Abraham solvation parameters are also given here. This combined model provide a generally trained model to predict the solubility of benzoic acid in a given cosolvent + water mixtures.

$$\begin{aligned} \ln x_{m,T} &= w_1 (A_1 + \frac{B_1}{T}) + w_2 (A_2 + \frac{B_2}{T}) \\ &+ (\frac{w_1 w_2}{T}) \begin{cases} J_1 + J_2 (c_1 - c_2)^2 + J_3 (e_1 - e_2)^2 + J_4 (s_1 - s_2)^2 + J_5 (a_1 - a_2)^2 + J_6 (b_1 - b_2)^2 \\ + J_7 (v_1 - v_2)^2 + J_8 (a_1 - a_2)^2 (b_1 - b_2)^2 \end{cases} \end{aligned}$$

$$\begin{aligned} &+ (\frac{w_1 w_2 (w_1 - w_2)}{T}) \begin{cases} J_9 + J_{10} (c_1 - c_2)^2 + J_{11} (e_1 - e_2)^2 + J_{12} (s_1 - s_2)^2 + J_{13} (a_1 - a_2)^2 \\ + J_{14} (b_1 - b_2)^2 + J_{15} (v_1 - v_2)^2 + J_{16} (a_1 - a_2)^2 (b_1 - b_2)^2 \end{cases} \end{aligned}$$
Eq. (10)
$$\begin{aligned} &+ (\frac{w_1 w_2 (w_1 - w_2)^2}{T}) \begin{cases} J_{17} + J_{18} (c_1 - c_2)^2 + J_{19} (e_1 - e_2)^2 + J_{20} (s_1 - s_2)^2 + J_{21} (a_1 - a_2)^2 \\ + J_{22} (b_1 - b_2)^2 + J_{23} (v_1 - v_2)^2 + J_{24} (a_1 - a_2)^2 (b_1 - b_2)^2 \end{cases} \end{aligned}$$

$$\begin{aligned} \ln x_{m,T} &= w_1 (4.183 - \frac{1766.916}{T}) + w_2 (11.783 - \frac{5095.935}{T}) \\ &+ (\frac{w_1 w_2}{T}) \left\{ 1265.197 + 27.334 \ (a_1 - a_2)^2 \right\} \\ &+ (\frac{w_1 w_2 (w_1 - w_2)}{T}) \left\{ \frac{-2524.032 \ (c_1 - c_2)^2 - 8081.901 \ (e_1 - e_2)^2}{-100.578 \ (a_1 - a_2)^2} \right\} \end{aligned}$$
 Eq. (11)  
$$&+ (\frac{w_1 w_2 (w_1 - w_2)^2}{T}) \left\{ \frac{405.686 \ (s_1 - s_2)^2 + 134.302 \ (a_1 - a_2)^2}{-9.898 \ (a_1 - a_2)^2 (b_1 - b_2)^2} \right\}$$

# **Conflict of interests**

The authors claim that there is no conflict of interest.

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